

Al-Ayen University  
College of Petroleum Engineering

# Reservoir Engineering II

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**Lecture 17: Water Influx (Part 1)**

Ref.: Reservoir Engineering Handbook by Tarek Ahmed

# Outline

- ❑ Introduction
  
- ❑ Classification of Aquifers
  - Degree of Pressure Maintenance
  - Outer Boundary Conditions
  - Flow Regimes
  - Flow Geometries
  
- ❑ Water Influx Models
  
- ❑ The Pot Aquifer Model

# Introduction

- Nearly all hydrocarbon reservoirs are surrounded by water-bearing rocks called *aquifers*.
- These aquifers may be substantially larger than the oil or gas reservoirs they adjoin as to appear infinite in size, or they may be so small in size as to be negligible in their effect on reservoir performance.
- Many gas and oil reservoirs produced by a mechanism termed *water drive*. Often this is called *natural water drive* to distinguish it from *artificial water drive* that involves the injection of water into the formation.
- Hydrocarbon production from the reservoir and the subsequent pressure drop prompt a response from the aquifer to offset the pressure decline.
- This response comes in a form of *water influx*, commonly called *water encroachment*.
- *Water encroachment* is attributed to:
  1. Expansion of the water in the aquifer
  2. Compressibility of the aquifer rock
  3. Artesian flow where the water-bearing formation outcrop is located structurally higher than the pay zone

# Classification of Aquifers

Reservoir-aquifer systems are commonly classified on the basis of:

- Degree of pressure maintenance
- Flow regimes
- Outer boundary conditions
- Flow geometries

## Degree of Pressure Maintenance

Based on the degree of the reservoir pressure maintenance provided by the aquifer, the natural water drive is often qualitatively described as:

- Active water drive
  - Partial water drive
  - Limited water drive
- The term *active* water drive refers to the water encroachment mechanism in which the rate of water influx equals the reservoir *total* production rate.

$$\left[ \begin{array}{c} \text{water influx} \\ \text{rate} \end{array} \right] = \left[ \begin{array}{c} \text{oil flow} \\ \text{rate} \end{array} \right] + \left[ \begin{array}{c} \text{free gas} \\ \text{flow rate} \end{array} \right] + \left[ \begin{array}{c} \text{water production} \\ \text{rate} \end{array} \right]$$

$$\left[ \begin{array}{c} \text{water influx} \\ \text{rate} \end{array} \right] = \left[ \begin{array}{c} \text{oil flow} \\ \text{rate} \end{array} \right] + \left[ \begin{array}{c} \text{free gas} \\ \text{flowrate} \end{array} \right] + \left[ \begin{array}{c} \text{water production} \\ \text{rate} \end{array} \right]$$

or

$$e_w = Q_o B_o + Q_g B_g + Q_w B_w$$

$$e_w = \frac{dW_e}{dt} = B_o \frac{dN_p}{dt} + (GOR - R_s) \frac{dN_p}{dt} B_g + \frac{dW_p}{dt} B_w$$

where

$e_w$  = water influx rate, bbl/day

$Q_o$  = oil flow rate, STB/day

$B_o$  = oil formation volume factor, bbl/STB

$Q_g$  = **free** gas flow rate, scf/day

$B_g$  = gas formation volume factor, bbl/scf

$Q_w$  = water flow rate, STB/day

$B_w$  = water formation volume factor, bbl/STB

$W_e$  = cumulative water influx, bbl

$t$  = time, days

$N_p$  = cumulative oil production, STB

GOR = current gas-oil ratio, scf/STB

$R_s$  = current gas solubility, scf/STB

$B_g$  = gas formation volume factor, bbl/scf

$W_p$  = cumulative water production, STB

$dN_p/dt$  = daily oil flow rate  $Q_o$ , STB/day

$dW_p/dt$  = daily water flow rate  $Q_w$ , STB/day

$dW_g/dt$  = daily water influx rate  $e_w$ , bbl/day

$(GOR - R_s) dN_p/dt$  = daily free gas flow rate, scf/day

## Example

Calculate the water influx rate  $e_w$  in a reservoir whose pressure is stabilized at 3000 psi.

Given: initial reservoir pressure = 3500 psi

$$dN_p/dt = 32,000 \text{ STB/day}$$

$$B_o = 1.4 \text{ bbl/STB}$$

$$\text{GOR} = 900 \text{ scf/STB}$$

$$R_s = 700 \text{ scf/STB}$$

$$B_g = 0.00082 \text{ bbl/scf}$$

$$dW_p/dt = 0$$

$$B_w = 1.0 \text{ bbl/STB}$$

## Solution

$$e_w = \frac{dW_e}{dt} = B_o \frac{dN_p}{dt} + (\text{GOR} - R_s) \frac{dN_p}{dt} B_g + \frac{dW_p}{dt} B_w$$

$$\begin{aligned} e_w &= (1.4) (32,000) + (900 - 700) (32,000) (0.00082) + 0 \\ &= 97,280 \text{ bbl/day} \end{aligned}$$

## Outer Boundary Conditions

The aquifer can be classified as infinite or finite (bounded).

- a. Infinite system indicates that the effect of the pressure changes at the oil/aquifer boundary can never be felt at the outer boundary. This boundary is for all intents and purposes at a constant pressure equal to initial reservoir pressure.
- b. Finite system indicates that the aquifer outer limit is affected by the influx into the oil zone and that the pressure at this outer limit changes with time.

## Flow Regimes

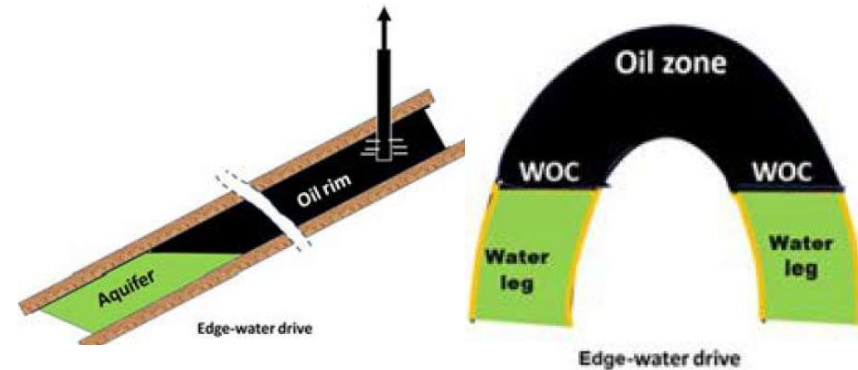
There are basically three flow regimes that influence the rate of water influx into the reservoir. As previously described, those flow regimes are:

- a. Steady-state
- b. Semisteady (pseudosteady)-state
- c. Unsteady-state

## Flow Geometries

### ■ Edge-water drive

- Water moves into the flanks of the reservoir
- Water flow is radial and lateral (negligible vertical flow)



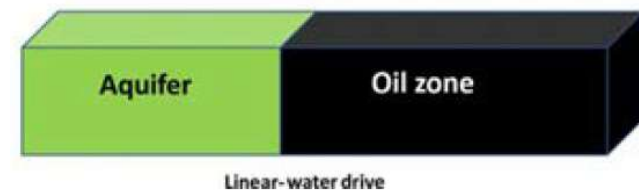
### ■ Bottom-water drive

- Reservoir in contact with aquifer throughout its areal extent
- Water flow is radial and vertical (significant vertical flow)



### ■ Linear-water drive

- Water influx from one flank of the reservoir
- Strictly linear with constant cross-sectional area





# Water Influx Models

The mathematical water influx models that are commonly used in the petroleum industry include:

- Pot aquifer
- Schilthuis' steady-state
- Hurst's modified steady-state
- The Van Everdingen-Hurst unsteady-state
  - Edge-water drive
  - Bottom-water drive
- The Carter-Tracy unsteady-state
- Fetkovich's method
  - Radial aquifer
  - Linear aquifer

## The Pot Aquifer Model

- The simplest model that can be used to estimate the water influx into a gas or oil reservoir.
- The model is based on the basic definition of compressibility.
- A drop in the reservoir pressure, due to the production of fluids, causes the aquifer water to expand and flow into the reservoir.

The compressibility is defined mathematically as:

$$\Delta V = c V \Delta p$$

Applying the above basic compressibility definition to the aquifer gives:

Water influx = (aquifer compressibility) (initial volume of water) (pressure drop)

or  $W_e = (c_w + c_f) W_i (p_i - p)$

where  $W_e$  = cumulative water influx, bbl

$c_w$  = aquifer water compressibility,  $\text{psi}^{-1}$

$c_f$  = aquifer rock compressibility,  $\text{psi}^{-1}$

$W_i$  = initial volume of water in the aquifer, bbl

$p_i$  = initial reservoir pressure, psi

$p$  = current reservoir pressure (pressure at oil-water contact), psi

Assuming the aquifer shape is radial, then:

$$W_i = \left[ \frac{\pi(r_a^2 - r_e^2)h\phi}{5.615} \right]$$

$r_a$  = radius of the aquifer, ft  
 $r_e$  = radius of the reservoir, ft  
 $h$  = thickness of the aquifer, ft  
 $\phi$  = porosity of the aquifer

Where the effective radius of the reservoir is expressed in terms of the reservoir pore volume “ $V_P$ ” as given by:

$$r_e = \sqrt{\frac{360 V_P}{\pi h \phi \theta}}$$

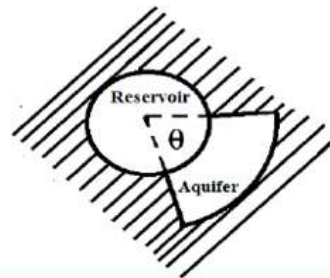
Where reservoir pore volume “ $V_P$ ” is expressed in  $\text{ft}^3$ .

- Quite often, water does not encroach on all sides of the reservoir, or the reservoir is not circular in nature. To account for these cases, a modification to the first Equation must be made:

$$W_e = (c_w + c_f) W_i f (p_i - p)$$

where the fractional encroachment angle  $f$  is defined by:

$$f = \frac{(\text{encroachment angle})^\circ}{360^\circ} = \frac{\theta}{360^\circ}$$



- The above model is only applicable to a small aquifer, i.e., pot aquifer, whose dimensions are of the same order of magnitude as the reservoir itself.

## Example

Calculate the cumulative water influx that results from a pressure drop of 200 psi at the oil-water contact with an encroachment angle of  $80^\circ$ . The reservoir-aquifer system is characterized by the following properties:

	Reservoir	Aquifer
radius, ft	2600	10,000
porosity	0.18	0.12
$c_f$ , $\text{psi}^{-1}$	$4 \times 10^{-6}$	$3 \times 10^{-6}$
$c_w$ , $\text{psi}^{-1}$	$5 \times 10^{-6}$	$4 \times 10^{-6}$
h, ft	20	25

## Solution

$$W_i = \left[ \frac{\pi(r_a^2 - r_e^2)h\phi}{5.615} \right] = \left( \frac{\pi(10,000^2 - 2600^2)(25)(0.12)}{5.615} \right) = 156.5 \text{ MMbbl}$$

$$W_e = (c_w + c_f) W_i f(p_i - p) = (4 + 3) 10^{-6} (156.5 \times 10^6) \left( \frac{80}{360} \right) (200) = 48,689 \text{ bbl}$$

***THANK YOU***